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(54) Orthopaedic apparatus for controlled contraction of soft tissue

Orthopädische Vorrichtung zur kontrollierten Kontraktion von weichem Gewebe

Appareil orthopédique permettant la contraction contrôlée des tissus mous

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EP 0 760 626 B1

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Description**BACKGROUND OF THE INVENTION****Field of the Invention**

[0001] This invention relates generally to the contraction of soft tissue, and more particularly, to the contraction of soft collagen tissue with minimal dissociation of collagen tissue.

Description of the Related Art

[0002] Instability of peripheral joints has long been recognized as a significant cause of disability and functional limitation in patients who are active in their daily activities, work or sports. Diarthrodial joints of musculoskeletal system have varying degrees of intrinsic stability based on joint geometry and ligament and soft tissue investment. Diarthrodial joints are comprised of the articulation of the ends of bones and their covering of hyaline cartilage surrounded by a soft tissue joint capsule that maintains the constant contact of the cartilage surfaces. This joint capsule also maintains within the joint the synovial fluid that provides nutrition and lubrication of the joint surfaces. Ligaments are soft tissue condensations in or around the joint capsule that reinforce and hold the joint together while also controlling and restricting various movements of the joints. The ligaments, joint capsule, and connective tissue are largely comprised of collagen.

[0003] When a joint becomes unstable, its soft tissue or bony structures allow for excessive motion of the joint surfaces relative to each other and in directions not normally permitted by the ligaments or capsule. When one surface of a joint slides out of position relative to the other surface, but some contact remains, subluxation occurs. When one surface of the joint completely disengages and loses contact with the opposing surface, a dislocation occurs. Typically, the more motion a joint normally demonstrates, the more inherently loose the soft tissue investment is surrounding the joint. This makes some joints more prone to instability than others. The shoulder, (glenohumeral) joint, for example, has the greatest range of motion of all peripheral joints. It has long been recognized as having the highest subluxation and dislocation rate because of its inherent laxity relative to more constrained "ball and socket" joints such as the hip.

[0004] Instability of the shoulder can occur congenitally, developmentally, or traumatically and often becomes recurrent, necessitating surgical repair. In fact subluxations and dislocations are a common occurrence and cause for a large number of orthopedic procedures each year. Symptoms include pain, instability, weakness, and limitation of function. If the instability is severe and recurrent, functional incapacity and arthritis may result. Surgical attempts are directed toward tight-

ening the soft tissue restraints that have become pathologically loose. These procedures are typically performed through open surgical approaches that often require hospitalization and prolonged rehabilitation programs.

[0005] More recently, endoscopic (arthroscopic) techniques for achieving these same goals have been explored with variable success. Endoscopic techniques have the advantage of being performed through smaller incisions and therefore are usually less painful, performed on an outpatient basis, are associated with less blood loss and lower risk of infection and have a more cosmetically acceptable scar. Recovery is often faster postoperatively than using open techniques. However, it is often more technically demanding to advance and tighten capsule or ligamentous tissue arthroscopically because of the difficult access to pathologically loose tissue and because it is very hard to determine how much tightening or advancement of the lax tissue is clinically necessary. In addition, fixation of advanced or tightened soft tissue is more difficult arthroscopically than through open surgical methods.

[0006] Collagen connective tissue is ubiquitous in the human body and demonstrates several unique characteristics not found in other tissues. It provides the cohesiveness of the musculoskeletal system, the structural integrity of the viscera as well as the elasticity of integument. These are basically five types of collagen molecules with Type I being most common in bone, tendon, skin and other connective tissues, and Type III is common in muscular and elastic tissues.

[0007] Intermolecular cross links provide collagen connective tissue with unique physical properties of high tensile strength and substantial elasticity. A previously recognized property of collagen is hydrothermal shrinkage of collagen fibers when elevated in temperature. This unique molecular response to temperature elevation is the result of rupture of the collagen stabilizing cross links and immediate contraction of the collagen fibers to about one-third of their original lineal distention. Additionally, the caliber of the individual fibers increases greatly, over four fold, without changing the structural integrity of the connection tissue.

[0008] There has been discussion in the existing literature regarding alteration of collagen connective tissue in different parts of the body. One known technique for effective use of this knowledge of the properties of collagen is through the use of infrared laser energy to effect tissue heating. The use of infrared laser energy as a corneal collagen shrinking tool of the eye has been described and relates to laser keratoplasty, as set forth in U.S. Patent No. 4,976,709. The importance controlling the localization, timing and intensity of laser energy delivery is recognized as paramount in providing the desired soft tissue shrinkage effects without creating excessive damage to the surrounding non-target tissues.

[0009] Radiofrequency (RF) electrical current has been used to reshape the cornea. Such shaping has

been reported by Doss in U.S. Patents No. 4,326,529; and 4,381,007. However, Doss was not concerned with dissociating collagen tissue in his reshaping of the cornea.

[0010] Shrinkage of collagen tissue is important in many applications. One such application is the shoulder capsule. The capsule of the shoulder consists of a synovial lining and three well defined layers of collagen. The fibers of the inner and outer layers extend in a coronal access from the glenoid to the humerus. The middle layer of the collagen extends in a sagittal direction, crossing the fibers of the other two layers. The relative thickness and degree of intermingling of collagen fibers of the three layers vary with different portions of the capsule. The ligamentous components of the capsule are represented by abrupt thickenings of the inner layer with a significant increase in well organized coarse collagen bundles in the coronal plane.

[0011] The capsule functions as a hammock-like sling to support the humeral head. In pathologic states of recurrent traumatic or developmental instability this capsule or pouch becomes attenuated and the capsule capacity increases secondary to capsule redundancy. In cases of congenital or developmental multi-directional laxity, an altered ratio of type I to type III collagen fibers may be noted. In these shoulder capsules a higher ratio of more elastic type III collagen has been described.

[0012] There is a need for an apparatus to effect controlled lineal contraction or shrinkage of collagen fibers to provide a multitude of nondestructive and beneficial structural changes and corrections within the body. More particularly with regard to the shoulder capsule, current surgical techniques involve cutting or advancing the shoulder capsule to eliminate capsular redundancy or to otherwise tighten the ligamous complex. Accordingly, there is a need to control shrinkage of the capsule by utilizing the knowledge of the properties of collagen in response to a specific level of thermal application.

SUMMARY OF THE INVENTION

[0013] According to the present invention, there is provided an orthopaedic apparatus as set out in claim 1.

[0014] Preferred features of the invention are set out in the dependent claims.

[0015] Because of the insulation layer, thermal energy is only delivered to the intended tissue, and not to tissue in an adjacent relationship to the area of treatment.

[0016] In certain instances it is desirable to be able to vary the length of the energy delivery surface which delivers the thermal energy to the tissue. For this purpose, an adjustable insulator, that is capable of movement along the longitudinal axis of the electrode, provides a way of adjusting the length of energy delivery surface.

[0017] Memory metals can be used for the construction of the electrode (energy delivery means). An advantage of memory metals is that with the application of heat to the metal, it can be caused to be deflected. This is

particularly useful for deflecting the distal end of the electrode.

[0018] The electrode can include a central lumen that receives an electrolytic solution from an electrolytic source. A plurality of apertures are formed in the distal end of the electrode and deliver the flowing electrolytic fluid to the tissue. Instead of an electrolytic solution, an electrolytic gel can also be introduced through the electrode.

[0019] In one embodiment of the invention, the insulation layer is a housing which positions the energy delivery surface in an adjacent but spaced relationship to the tissue. A portion of the insulating housing rides on the tissue, and creates the equivalent of a partial dam for electrolytic solution introduced through the electrode and towards the tissue. A cuff is disposed about the insulating housing. The cuff and insulating housing together create a return electrolytic solution channel for the removal of solution flowing out of the dam and away from the tissue site.

[0020] The handpiece of the invention can be connected, with a cable, to an RF energy source. A closed loop feedback system can be included and coupled to a temperature sensor on the electrode and the RF energy source. Temperature at the electrode can be monitored, and the power of the RF energy source adjusted to control the amount of energy that is delivered to the tissue.

[0021] The present invention has wide spread application to many different anatomical locations. It can be utilized for controlled contraction of collagen soft tissue of a joint capsule, particularly the gleno-humeral joint capsule of the shoulder, to treat herniated discs, the meniscus of the knee, to name just a few.

[0022] In one embodiment of the invention, RF heating in a fluid or saline environment is used to control thermal spread to soft collagen tissue. The RF energy can be delivered through an endoscopically guided handpiece under arthroscopic visualization by the surgeon. In the temperature range of 43 to 90 degrees C, maximum collagen contraction is achieved. Additional temperature ranges are 43 to 75 degrees C, and 45 to 60 degrees C. Lower temperatures do not provide maximum thermal induced contracture of the collagen fibrils. Greater temperatures create excessive destruction and disintegration of the collagen fibrillar pattern. Thus, the present invention provides apparatus which accurately controls the application of heat within a desired thermal range. This heat is delivered to the collagen soft tissue, thereby contracting and restricting the soft tissue elasticity and improving stability.

DESCRIPTION OF THE DRAWINGS

[0023]

[0024] Figure 1 is a perspective plan view of an apparatus for controlled contraction of tissue that includes collagen fibers, including a handpiece and an electrode,

according to the invention.

[0025] Figure 2 is a perspective plan view of a distal end of the electrode with all edges radiused according to the invention.

[0026] Figure 3 is a side view of the distal end of the electrode of Figure 2.

[0027] Figure 4 is a sectional view of the deflected electrode with a resistive heating element positioned in an interior lumen of the electrode according to the invention.

[0028] Figure 5 is a perspective plan view of the apparatus for controlled contraction of tissue with collagen fibers with a handpiece, electrode and an operating cannula according to the present invention.

[0029] Figure 6 is a close up perspective plan view of the distal end of the electrode of the apparatus of Figure 5 according to the invention.

[0030] Figure 7 is a perspective plan view of an electrode with a steering wire positioned on the exterior of the electrode according to the invention.

[0031] Figure 8 is a sectional view of an electrode with a lumen and a plug that is attached to the electrode distal end according to the invention.

[0032] Figure 9 is a cross sectional view of an electrode with fluid flowing through an interior lumen of the electrode according to the invention.

[0033] Figure 10 is a cross sectional view of an RF electrode structure with an insulating housing surrounding a portion of an electrode, and a cuff surrounding the insulating housing according to the invention.

[0034] Figure 11 is a block diagram of a fluid control system useful with the electrode structure of Figure 10 according to the invention.

[0035] Figure 12 is a perspective plan view of a handpiece, an electrode and a sleeve that slides across the surface of the electrode to vary the amount of electrode conductive surface according to the invention.

[0036] Figure 13 is a sectional view of an electrode with an oval cross section and the heating zone in the tissue according to the invention.

[0037] Figure 14 is a sectional view of a handle, electrode, operating cannula and a viewing scope, with the viewing scope and electrode positioned in the operating cannula according to the invention.

[0038] Figure 15 is a cross sectional view of the device of Figure 14, taken along the lines 15-15 according to the invention.

[0039] Figure 16 is a perspective plan view of an electrode distal end with temperature sensors positioned in the distal end according to the invention.

[0040] Figure 17 is a block diagram of a closed loop feedback system according to the invention.

[0041] Figure 18 is a perspective plan view of a roller element mounted at an electrode distal end according to the invention.

[0042] Figure 19 is a drawing of the right glenohumeral capsuloligamentous complex.

[0043] Figure 20 is a drawing of a loose joint capsule.

[0044] Figure 21 is a schematic drawing of the apparatus of the invention with an electrode supplying thermal energy to a joint structure.

[0045] Figure 22 is a sectional view of a disc positioned between two vertebrae.

[0046] Figure 23 is a schematic drawing of the apparatus of the invention with an electrode supplying thermal energy to a herniated disc.

10 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0047] Referring now generally to Figure 1, an apparatus for controlled contraction of tissue that includes 15 collagen fibers is generally denoted as 10. Apparatus 10 includes a handpiece 12 that is preferably made of an insulating material. Types of such insulating materials are well known by those skilled in the art. An electrode 14 is associated with handle 12 at a proximal end 20 of electrode 14.

[0048] A distal end 18 of electrode 14 has a geometry that delivers a controlled amount of energy to the tissue in order to achieve a desired level of contraction of the collagen fibers. Contraction is achieved while dissociation and breakdown of the collagen fibers is minimized.

[0049] Electrode 14 can have a flat elongated structure that is easily painted across a tissue without "hanging up" on any section of the tissue. In one geometry of electrode 14, all edges 20 of distal end 18 are radiused, 30 as illustrated in Figures 2 and 3. Distal end 18 can have a variety of geometric configurations. One such geometry is a disc shaped geometry without square edges. Electrode 14 can be made of a number of different materials including but not limited to stainless steel, platinum, other noble metals and the like. Electrode 14 can be made of a memory metal, such as nickel titanium, commercially available from Raychem Corporation, Menlo Park, California. In Figure 4, a resistive heating element 22 is positioned in an interior lumen of electrode

35 14. Resistive heating element can be made of a suitable metal that transfers heat to electrode 14, causing electrode distal end 18 to become deflected when the temperature of electrode 14 reaches a level that the memory metal is caused to deflect, as is well known in the art.

[0050] Not all of electrode 14 need be made of the memory metal. It is possible that only electrode distal end 18 be made of the memory metal in order to effect the desired deflection. There are other methods of deflecting electrode 18, as will be more fully discussed and described 45 in a later section of this specification.

[0051] Apparatus 10, comprising handpiece 12 and electrode 14, is adapted to be introduced through an operating cannula for percutaneous applications. It will be appreciated that apparatus 10 may also be used in non-

55 percutaneous applications and that an operating cannula is not necessary in the broad application of the invention.

[0052] As illustrated in Figures 5 and 6, apparatus 10

can also include, as an integral member, an operating cannula 24 which can be in the form of a hypodermic trocar with dimensions of about 3 to 6 mm outside diameter, with tubular geometries such as those of standard commercially available operating cannulas. Operating cannula 24 can be made of a variety of biocompatible materials including but not limited to stainless steel, and the like.

[0052] Operating cannula 24 has a proximal end that attaches to handpiece 12 and it can have a sharp or piercing distal end 26 that pierces a body structure in order to introduce electrode 14 to a desired site. Electrode 14 is positioned within an interior lumen of operating cannula 24 and is extendable beyond distal end 26 in order to reach the desired tissue site. Electrode 14 can be advanced and retracted in and out of operating cannula 24 by activating a deployment button 28 which is located on the exterior of handle 12. Deployment button 28 is preferably activated by the operator merely by sliding it, which causes electrode 14 to advance in a direction away from distal end 26 of operating cannula 24. Deployment button 28 can be pulled back, causing a retraction of electrode 14 towards distal end 26. In many instances, electrode 14 will be retracted to be positioned entirely within operating cannula 24. Electrode 14 can also be deployed with fluid hydraulics, pneumatics, servo motors, linear actuators, and the like.

[0053] An electrical and/or fluid flow cable 28 attaches to handle 12 and provides the necessary connection of apparatus 10 to a suitable energy source and/or a source of fluid, which may be an electrolytic solution or an electrolytic gel. An electrolytic solution, for purposes of this invention, is one that increases the transfer of thermal energy from electrode 14 to a tissue. Suitable electrolytic solutions include but are not limited to saline solution and the like.

[0054] A variety of energy sources can be used with the present invention to transfer thermal energy to the tissue that includes collagen fibers. Such energy sources include but are not limited to RF, microwave, ultrasonic, coherent light and thermal transfer.

[0055] When an RF energy source is used, the physician can activate the energy source by the use of a foot switch 30 that is associated with handle 12 and electrode 14. Significantly, a controlled amount of RF energy is delivered so that there is an effective transfer of thermal energy to the tissue site so that the thermal energy spreads widely through the tissue but does not cause a dissociation or breakdown of the collagen fibers.

[0056] For many applications, it is necessary to have electrode distal end 18 become deflected (Figure 6). This can be achieved with the use of memory metals, or it can be accomplished mechanically. A steering wire, or other mechanical structure, is attached to either the exterior or interior of electrode 14. A deflection button 32, located on handle 12, is activated by the physician, causing steering wire 34 (Figure 7) to tighten, and impart a retraction of electrode 14, resulting in a deflection of

electrode distal end 18. It will be appreciated that other mechanical mechanisms can be used in place of steering wire 34. The deflection may be desirable for tissue sites that have difficult access, and it is necessary to move about a non-linear tissue. By deflecting electrode distal end 18, the opportunity to provide more even thermal energy to a tissue site is achieved, and the possibility of ablating or dissociation of collagen material is greatly reduced.

[0057] As shown in Figure 7, steering wire 34 attaches to a flat formed on the exterior of electrode 14. Wire EDM technology can be used to form the flat on electrode 14. A "T" bar configuration is illustrated in Figure 7. Chemical etching may be used to create the "T" bar. Steering wire 34 need not be an actual wire. It can also be a high tensile strength cord such as Kevlar (trade mark). Steering wire 34 can be made of stainless steel flat wire, sheet material, and the like.

[0058] Electrode 14 can be tubular in nature with a central lumen. Electrode distal end 18 can include a conductive plug that is sealed to electrode distal end 18 by welding, e-beam, laser, and the like.

[0059] In Figure 9, electrode 14 includes an electrical insulation layer 38 formed on a back side of electrode 14 which is intended to minimize damage to tissue areas that are not treated. For example, when electrode 14 is introduced into a tight area, and only one surface of the tight area is to be treated, then it is desirable to avoid delivering thermal energy to other tissue site areas. The inclusion of insulation layer 38 accomplishes this result. Suitable insulation materials include but are not limited to polyimide, epoxy varnish, PVC and the like. Electrode 14 includes a conductive surface 40 which does not include insulation layer 38.

[0060] A plurality of apertures 42 are formed in electrode 14 to introduce a flowing fluid 44 through an interior lumen of electrode 14 and to the tissue site. The flowing fluid can be an electrolytic solution or gel, including but not limited to saline. The electrolyte furnishes an efficient electrical path and contact between electrode 14 and the tissue to be heated.

[0061] Referring now to Figure 10, electrode 14 includes a central lumen for receiving an electrolytic solution 44 from an electrolytic source. Electrolytic solution 44 flows from electrode 14 through a plurality of apertures 42 formed in conductive surface 40. An insulating housing 46 surrounds electrode 14, leaving only conductive surface 40 exposed. Insulating housing 46 can be formed of a variety of non-electrically conducting materials including but not limited to thermoplastics, thermosetting plastic resins, ceramics, and the like. Insulating housing 46 rides along the surface of the tissue to be treated and positions conductive surface 40 in an adjacent but spaced relationship with the tissue. In this manner, there isn't direct contact of conductive surface 40 with the tissue, and the chance of dissociation or break down of the collagen fibers is reduced. Insulating housing 46 creates a partial dam 48 of electrolytic solu-

tion adjacent to the tissue. Electrical energy is transferred from electrode 14 to electrolytic solution 44, and from electrolytic solution 44 in dam 48 to the tissue. A cuff 50 surrounds insulating housing 46. Cuff 50 may be made of a variety of materials including but not limited to thermoplastic, thermosetting plastic resins, ceramics and the like. The respective dimensions of insulating housing 46 and cuff can vary according to the specific application.

[0062] Cuff 50 and insulating housing 46 are closely positioned to each other, but they are spaced in a manner to create a return electrolytic solution channel 52. The used electrolyte solution may either be released within a confined body area, such as the joint, or not be returned to the tissue, but instead is removed.

[0063] Use of a cooled solution to deliver the thermal energy to the tissue, instead of direct contact with conductive surface 40, provides a more even thermal gradient in the tissue. Avoidance of surface overheating can be accomplished. There is a more uniform level of thermal energy applied to the tissue. Electrolytic solution 44 may be cooled in the range of about 30 to 55 degrees C.

[0064] Referring now to Figure 11, electrolytic solution 44 is in a holding container 54 and transferred through a fluid conduit 56 to a temperature controller 58 which can cool and heat electrolytic solution 44 to a desired temperature. A pump 60 is associated with fluid conduit 56 to transfer fluid throughout the system and delivers electrolytic solution 44 through handpiece 12 to electrode 14. Returning electrolytic fluid 44 passes through return electrolytic solution channel 52, and is delivered to a waste container 62. The flow rate of electrolytic solution can be in the range of less than about 1cc/min. to greater than 5cc/second.

[0065] The area of electrode 14 that serves as conductive surface 44 can be adjusted by the inclusion of an insulating sleeve 64 (Figure 12) that is positioned around electrode 14. Sleeve 64 is advanced and retracted along the surface of electrode 14 in order to increase or decrease the surface area of conductive surface 44 that is directed to the tissue. Sleeve 64 can be made of a variety of materials including but not limited to nylon, polyimides, other thermoplastics and the like. The amount of available conductive surface 44 available to deliver thermal energy can be achieved with devices other than sleeve 64, including but not limited to printed circuitry with multiple circuits that can be individually activated, and the like.

[0066] Electrode 14 can have a variety of different geometric configurations. In one embodiment, electrode 14 has an oval cross section (Figure 13). The oval cross section provides a greater conductive surface 44 area that is in contact with the tissue. A larger zone of heating to the tissue is provided. The thermal gradient within the tissue is more even and the possible dissociation or breakdown of the collagen fibers is reduced.

[0067] As illustrated in Figure 14, operating cannula

24 includes a viewing scope 66 which may be positioned above electrode 14 (Figure 15). Viewing scope 66 provides a field of view 68, permitting the surgeon to view while delivering energy to the tissue site and contracting the tissue. Viewing scope 66 can include a bundle of light transmitting fibers and optical viewing elements. Alternatively, the surgeon can view the procedure under arthroscopic visualization.

[0068] Referring now to Figure 16, one or more temperature sensors 70 can be positioned in electrode 14, at electrode distal end 18. Temperature sensor 70 can be a thermocouple, a thermistor or phosphor coated optical fibers. Temperature sensor 70 can be utilized to determine the temperature of electrode 14, particularly at conductive surface 40, or temperature sensor 70 may be employed to determine the temperature of the tissue site.

[0069] Additionally, the apparatus of the present invention can be an RF energy delivery device to effect contraction of collagen soft tissue while minimizing dissociation or breakdown of the collagen fibers. As shown in Figure 17 the apparatus for controlled contraction of collagen soft tissue includes handpiece 12, electrode 14, operating cannula 24, a cable 28 and an RF power source 72. Suitable RF power sources are commercially available and well known to those skilled in the art. In one embodiment of the invention RF power source 72 has a single channel, delivering approximately 30 watts of RF energy and possessing continued flow capability.

[0070] A closed loop feedback system, coupling temperature sensor 70 to RF energy source 72 can be included. The temperature of the tissue, or of electrode 14 is monitored, and the power of RF generator 72 adjusted accordingly. The physician can, if desired, override the closed loop system. A microprocessor 74 can be included and incorporated into the closed loop system switch to power on and off, as well as to modulate the power. A suitable microprocessor is commercially available and well known to those skilled in the art of closed loop feedback systems. The closed loop system utilizes microprocessor 74 to serve as a controller, watch the temperature, adjust the RF power, look at the result, refed the result, and then modulate the power.

[0071] Optionally positioned on electrode distal end 18 is a conductive roller element 76 (Figure 18). Conductive roller element is rotatably mounted on electrode distal end 18 and can include a plurality of projections 78. Roller element 76 is moved across the tissue site, along with projections 78, to deliver the thermal energy.

[0072] The apparatus of the present invention allows contraction of collagen soft tissue. The collagen soft tissue is contracted to a desired shrinkage level without dissociation and breakdown of the collagen structure. It can be used in the shoulder, spine, and the like. It will be appreciated by those skilled in the art that the present invention has a variety of different applications, not merely those specifically mentioned in this specification. Some specific applications include joint capsules, spe-

cifically the gleno-humeral joint capsule of the shoulder, herniated discs, and the meniscus of the knee.

[0072] RF energy, thermal energy, is delivered to collagen soft tissue. The thermal energy penetrates more than 1 mm through the collagen soft tissue. The penetration can be as much as about 3 mm. Electrode 14 is painted across the collagen soft tissue sequentially until the maximum shrinkage occurs. In one embodiment, the collagen soft tissue is contracted in an amount of about two-thirds of its resting weight. A temperature range of about 43 to 90 degrees C is preferred. More preferred, the temperature range is about 43 to 75 degrees C. Still more preferred is a temperature range of 45 to 60 degrees C.

[0073] In one specific use of the invention, joint capsules are treated to eliminate capsular redundancy. More specifically, the invention is utilized to contract soft collagen tissue in the gleno-humoral joint capsule of the shoulder. The basic anatomy of the gleno-humeral joint capsule of the shoulder is illustrated in Figure 19.

[0074] The apparatus of the present invention may provide RF heating in a fluid or saline environment to control thermal spread. RF heating is applied to collagen connective tissue shrinkage in temperature ranges of about 43 to 90 degrees C, 43 to 75 degrees C and 45 to 60 degrees C. The RF energy is delivered through endoscopically guided handpiece 12 in a fluid or saline environment within the joint. It can be under arthroscopic visualization by the surgeon, or the apparatus can include a viewing device. The invention may accurately control the application of heat within a specific thermal range, and deliver thermal energy to collagen soft tissue of the joint, thereby contracting and restricting the soft tissue elasticity and improving joint stability. When applied to the shoulder, there is capsular shrinkage of the gleno-humoral joint capsule of the shoulder and a consequent contracture of the volume, the interior circumference, of the shoulder capsule to correct for recurrent instability symptoms. The degree of capsular shrinkage is determined by the operating surgeon, based on severity of preoperative symptoms and condition of the capsule at the time of arthroscopic inspection. The maximum amount of collagen contraction achieved is approximately two-thirds of its original structure.

[0075] In Figure 20, a loose capsule is illustrated. The apparatus for controlled contraction of tissue of the present invention is applied to a joint capsule (Figure 21). Electrode distal end 18 is painted across the surface of the collagen soft tissue. Figures 22 and 23 illustrate the application of the invention to a herniated disc.

Claims

1. An orthopaedic apparatus (10) for thermally contracting collagen fibers in an orthopaedic tissue, comprising:

energy delivery means (14) insertable percutaneously and including a proximal end (16), a distal end (18), an energy delivery surface (40) extending along a first ride at the distal end for delivering energy into the collagen fibers to thermally contract the collagen fibers and a thermal insulation layer (38, 46) extending along the reverse ride at the distal end; a handle means (12) coupled to the proximal end (16); and a cable means coupled to the energy delivery means (14) for delivering energy thereto.

- 15 2. The apparatus of claim 1, wherein the distal end
 (18) has a deflectable tip and the energy delivery
 means (14) further includes deflection means (32,
 34) operable to deflect the deflectable tip.

20 3. The apparatus of any preceding claim, wherein the
 energy delivery means (14) is an RF electrode
 means, the energy delivery surface is arranged to
 deliver RF energy into the collagen fibers to ther-
 mally contract the collagen fibers and the cable
 means is arranged to deliver RF energy to the RF
 25 electrode means (14).

30 4. The apparatus of any preceding claim, further com-
 prising:
 a feedback control system means (70, 74)
 coupled to the energy delivery means (14) for con-
 trolling the amount of energy delivered into the col-
 lagen fibers.

35 5. The apparatus of claim 4, wherein the feedback
 control system means (i) includes at least one tem-
 perature sensor (70) positioned at the distal end
 (18) for determining the temperature of tissue con-
 taining the collagen fibers and (ii) is arranged to
 40 control the delivery of energy to raise the tempera-
 ture of the collagen fibers to 43 to 90 degrees C.

45 6. The apparatus of claim 4, wherein the feedback
 control system means (i) includes at least one tem-
 perature sensor (70) positioned at the distal end
 (18) for determining the temperature of tissue con-
 taining the collagen fibers and (ii) is arranged to
 50 control the delivery of energy to raise the tempera-
 ture of the collagen fibers to 43 to 75 degrees C.

55 7. The apparatus of claim 4, wherein the feedback
 control system means (i) includes at least one tem-
 perature sensor (70) positioned at the distal end
 (18) for determining the temperature of tissue con-
 taining the collagen fibers and (ii) is arranged to
 60 control the delivery of energy to raise the tempera-
 ture of the collagen fibers to 45 to 60 degrees C.

65 8. The apparatus of any preceding claim, further com-

prising viewing means (66) for viewing tissue containing the collagen fibers.

Patentansprüche

- Orthopädische Vorrichtung (10) zum thermischen Kontrahieren von Kollagenfasern in einem orthopädischen Gewebe mit:

Energieliefermitteln (14), die perkutan einführbar sind und ein proximales Ende (16), ein distales Ende (18), eine Energielieferoberfläche (40), die sich längs einer ersten Seite an dem distalen Ende erstreckt für das Liefern von Energie in die Kollagenfasern, um diese thermisch zu kontrahieren, und eine thermische Isolierschicht (38, 46) aufweist, welche sich längs der umgekehrten Seite an dem distalen Ende erstreckt;

Handgriffmitteln (12), die mit dem proximalen Ende (16) gekoppelt sind; und

einem Kabelmittel, welches an das Energieliefermittel (14) zum Liefern von Energie an dieses gekoppelt ist.

- Vorrichtung nach Anspruch 1, wobei das distale Ende (18) eine ablenkbare Spitze hat und das Energieliefermittel (14) ferner Ablenkmittel (32, 34) aufweist, um betrieblich die ablenkbare Spitze abzulenken.
- Vorrichtung nach einem vorhergehenden Anspruch, wobei das Energieliefermittel (14) ein Radiofrequenz-Elektrodenmittel ist, die Energielieferfläche angeordnet ist, um Radiofrequenzenergie in die Kollagenfasern zu liefern und diese thermisch zu kontrahieren, und das Kabelmittel angeordnet ist, um RF-Energie zu dem RF-Elektrodenmittel (14) zu liefern.
- Vorrichtung nach einem vorhergehenden Anspruch, ferner mit einem Rückkopplungskontrollsystemmittel (70, 74), welches mit dem Energieliefermittel (14) gekoppelt ist zur Steuerung des Energiebetrages, welcher in die Kollagenfasern geliefert wird.
- Vorrichtung nach Anspruch 4, wobei das Rückkopplungssteuersystemmittel (i) mindestens einen Temperatursensor (70) aufweist, der an dem distalen Ende (18) für das Bestimmen der Temperatur des Gewebes angeordnet ist, welches die Kollagenfasern enthält, und (ii) angeordnet ist, um die Energielieferung zu steuern und die Temperatur der Kollagenfasern auf 43 bis 90°C anzuheben.

5 6. Vorrichtung nach Anspruch 4, wobei das Rückkopplungssteuersystemmittel (i) mindestens einen Temperatursensor (70) aufweist, der an dem distalen Ende (18) für das Bestimmen der Temperatur des Gewebes angeordnet ist, welches die Kollagenfasern enthält, und (ii) angeordnet ist, um das Liefern von Energie zu steuern und die Temperatur der Kollagenfasern auf 43 bis 75°C anzuheben.

10 7. Vorrichtung nach Anspruch 4, wobei das Rückkopplungssteuersystemmittel (i) mindestens einen Temperatursensor (70) aufweist, der an dem distalen Ende (18) für das Bestimmen der Temperatur des Gewebes angeordnet ist, welches die Kollagenfasern enthält, und (ii) angeordnet ist, um das Liefern von Energie zu steuern und die Temperatur der Kollagenfasern auf 45 bis 60°C anzuheben.

15 8. Vorrichtung nach einem vorhergehenden Anspruch, ferner mit Sichtmitteln (66) zum Betrachten des die Kollagenfasern enthaltenden Gewebes.

Revendications

- 25 1. Appareil orthopédique (10) pour contracter thermiquement des fibres de collagène dans un tissu orthopédique, comportant :
- 30 un moyen (14) de distribution d'énergie pouvant être inséré par voie percutanée et comprenant une extrémité proximale (16), une extrémité distale (18), une surface (40) de distribution d'énergie s'étendant le long d'un premier côté à l'extrémité distale pour distribuer de l'énergie dans les fibres de collagène afin de contracter thermiquement les fibres de collagène et une couche (38,46) d'isolation thermique s'étendant le long du côté opposé, à l'extrémité distale ;
- 35 un moyen à poignée (12) relié à l'extrémité proximale (16) ; et
- 40 un moyen à câble relié au moyen (14) de distribution d'énergie pour y distribuer de l'énergie.
- 45 2. Appareil selon la revendication 1, dans lequel l'extrémité distale (18) comporte une pointe pouvant fléchir et le moyen (14) de distribution d'énergie comprend en outre des moyens de flexion (32,34) pouvant être actionnés pour faire fléchir la pointe flexible.
- 50 3. Appareil selon l'une quelconque des revendications précédentes, dans lequel le moyen (14) de distribution d'énergie est un moyen à électrode RF, la surface de distribution d'énergie est agencée de façon à distribuer de l'énergie RF dans les fibres de col-

lagène pour contracter thermiquement les fibres de collagène et le moyen à câble est agencé de façon à distribuer de l'énergie RF au moyen (14) à électrode RF.

5

4. Appareil selon l'une quelconque des revendications précédentes, comportant en outre :

un moyen (70,74) à système de commande à rétro-action relié au moyen (14) de distribution d'énergie pour régler la quantité d'énergie distribuée dans les fibres de collagène.

10

5. Appareil selon la revendication 4, dans lequel le moyen (i) à système de commande à rétro-action comprend au moins un capteur de température (70) positionné à l'extrémité distale (18) pour déterminer la température d'un tissu contenant les fibres de collagène et (ii) est agencé de façon à commander la distribution d'énergie pour éléver la température des fibres de collagène à une valeur de 43 à 90 degrés C.

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6. Appareil selon la revendication 4, dans lequel le moyen à système de commande à rétro-action (i) comprend au moins un capteur (70) de température positionné à l'extrémité distale (18) pour déterminer la température d'un tissu contenant les fibres de collagène et (ii) est agencé de façon à commander la distribution d'énergie pour éléver la température des fibres de collagène à une valeur de 43 à 75 degrés C.

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7. Appareil selon la revendication 4, dans lequel le moyen à système de commande à rétro-action (i) comprend au moins un capteur (70) de température positionné à l'extrémité distale (18) pour déterminer la température d'un tissu contenant les fibres de collagène et (ii) est agencé de façon à commander la distribution d'énergie pour éléver la température des fibres de collagène à une valeur de 45 à 60 degrés C.

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8. Appareil selon l'une quelconque des revendications précédentes, comportant en outre un moyen d'observation (66) pour l'observation d'un tissu contenant les fibres de collagène.

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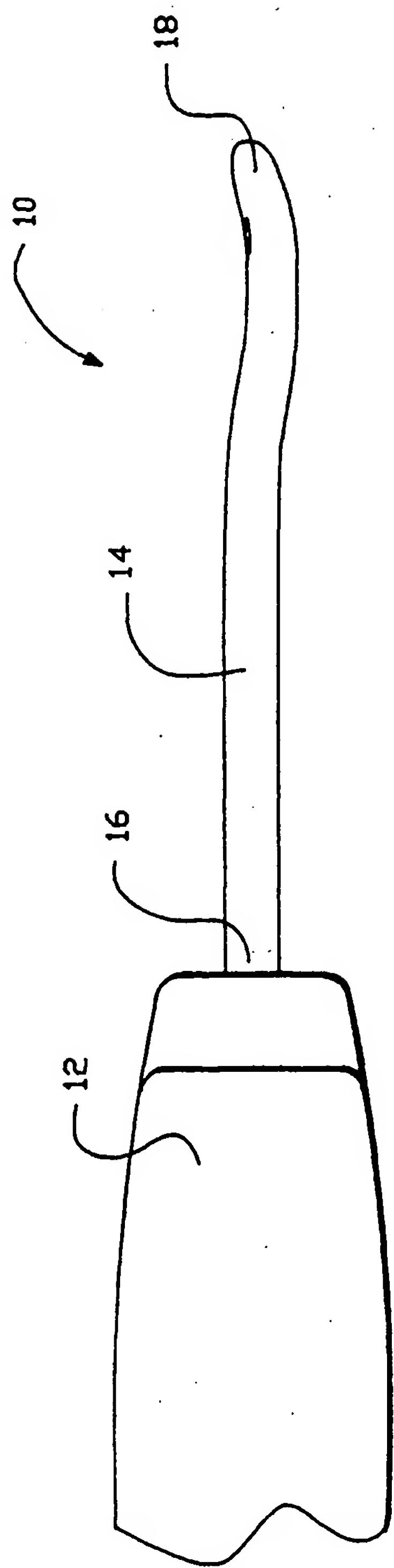


FIG. 1

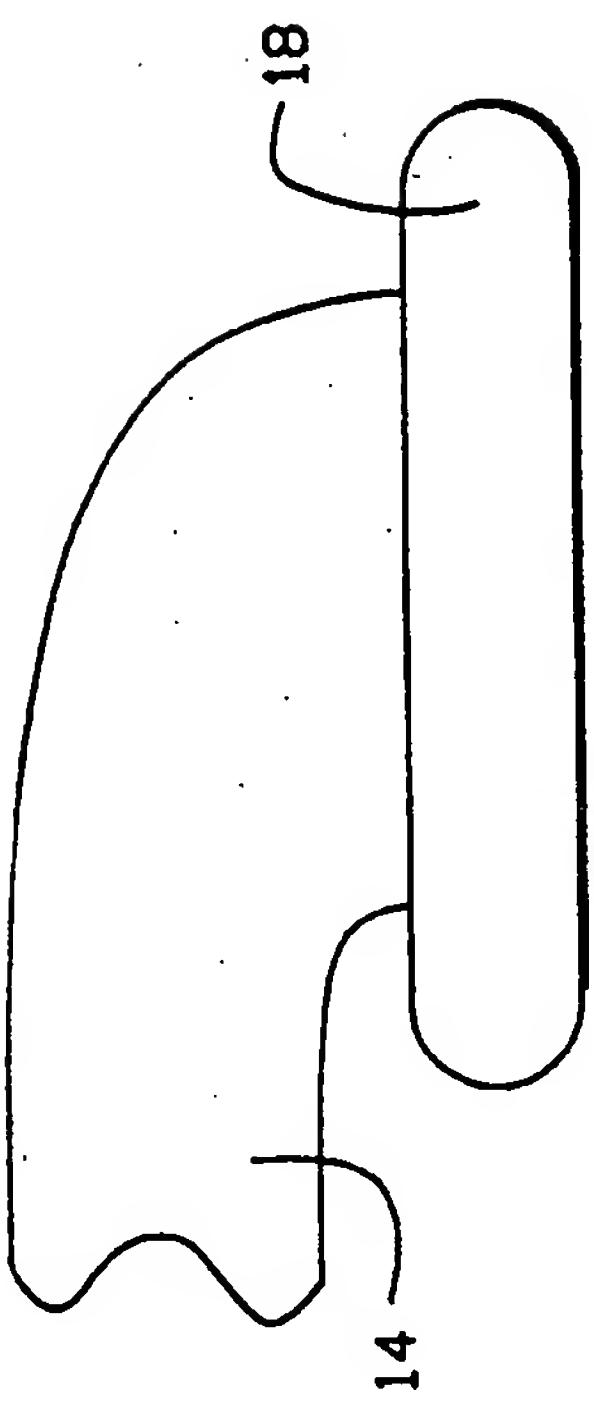


FIG. 3

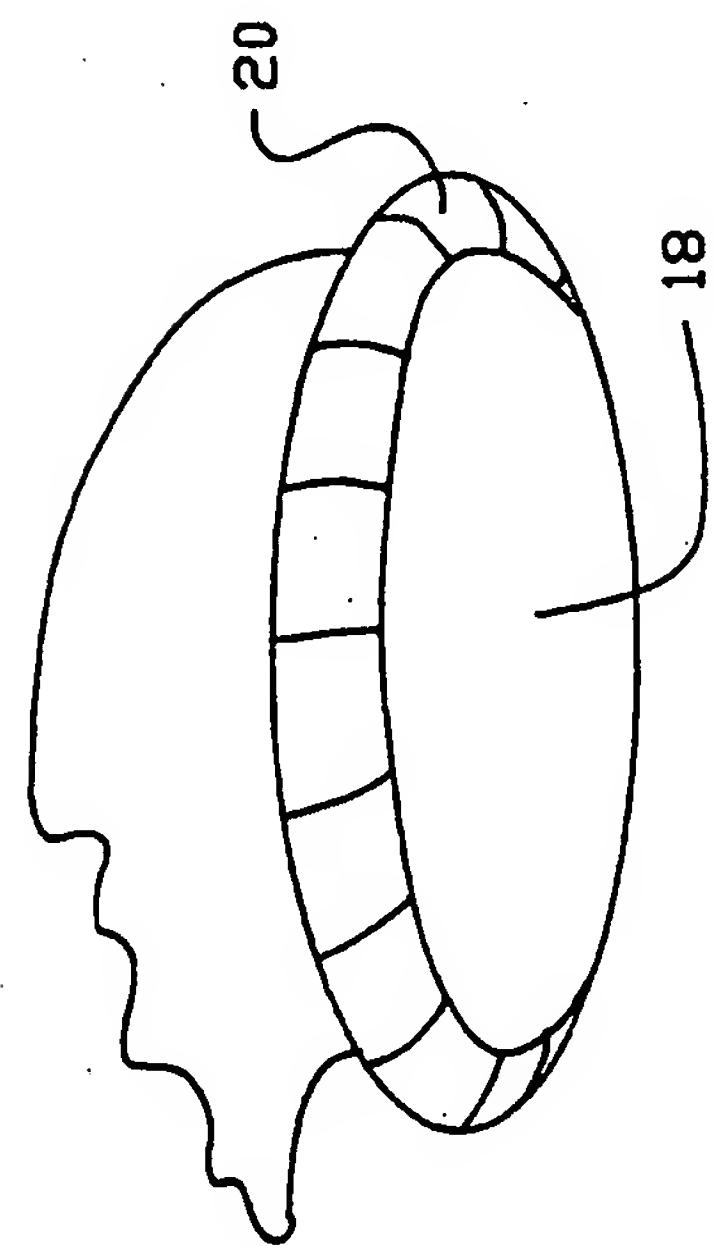


FIG. 2

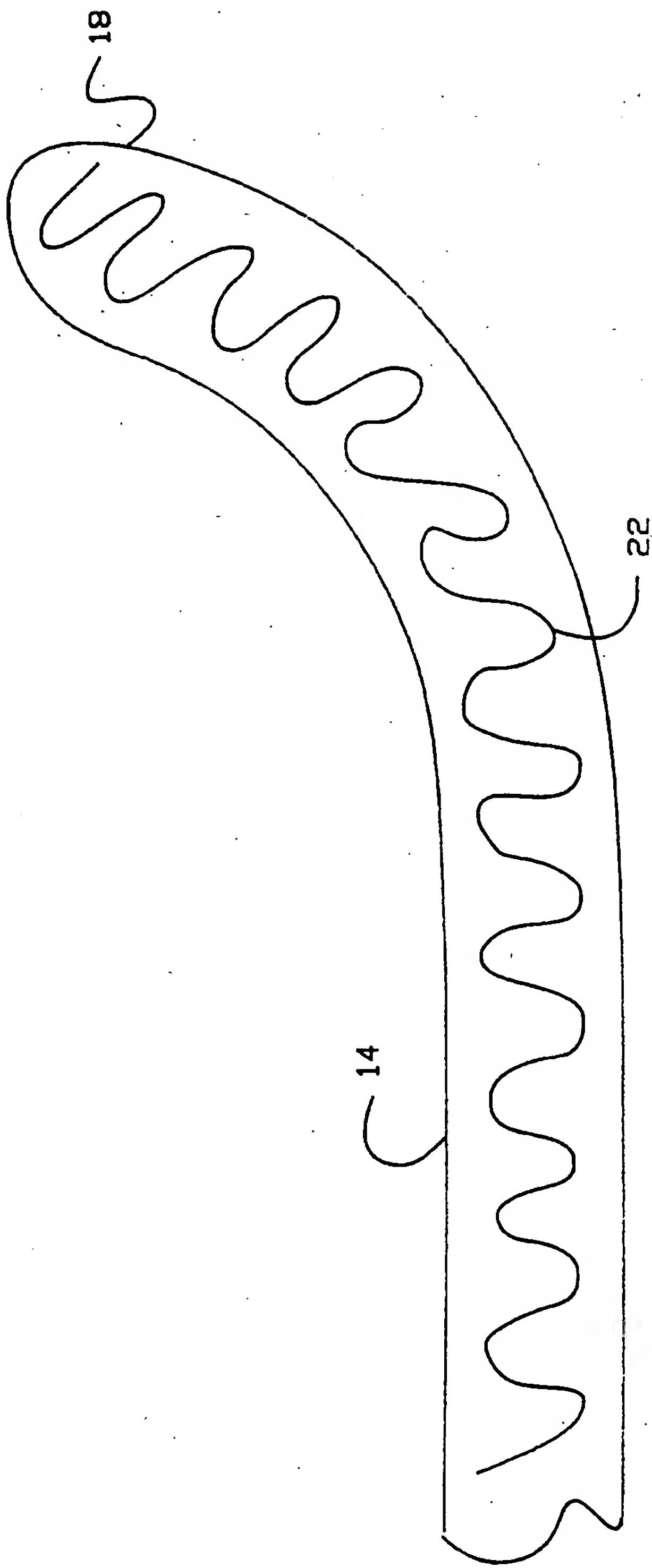


FIG. 4

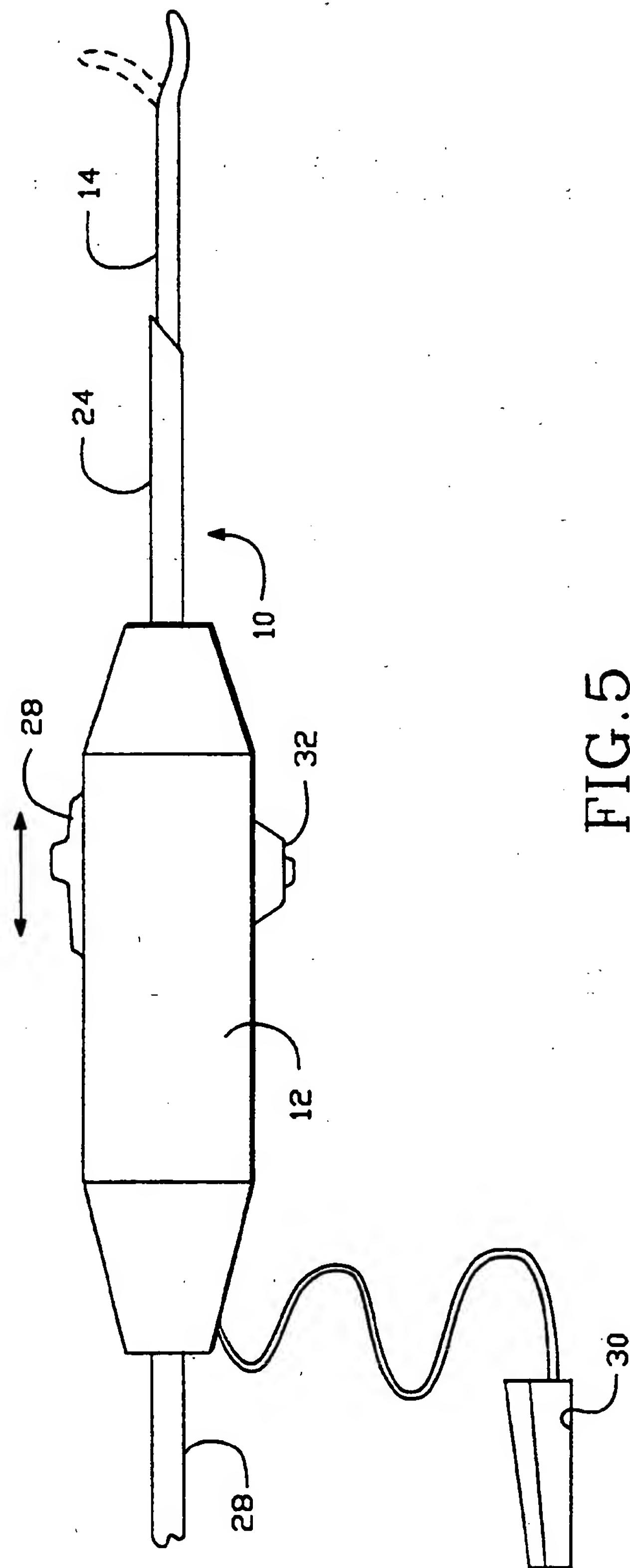


FIG. 5

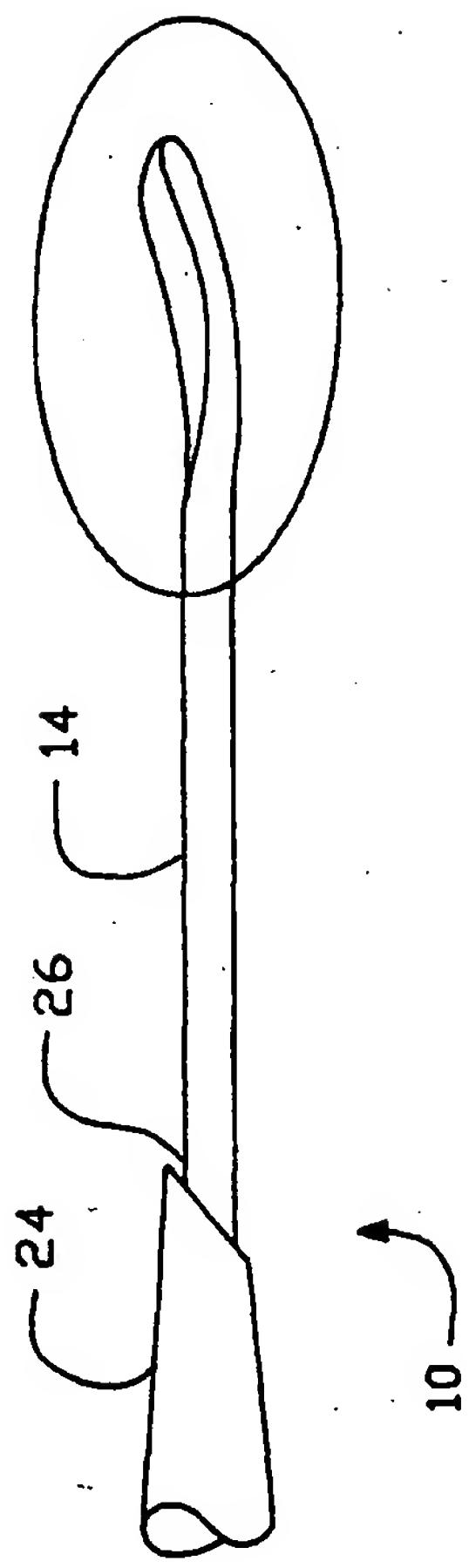
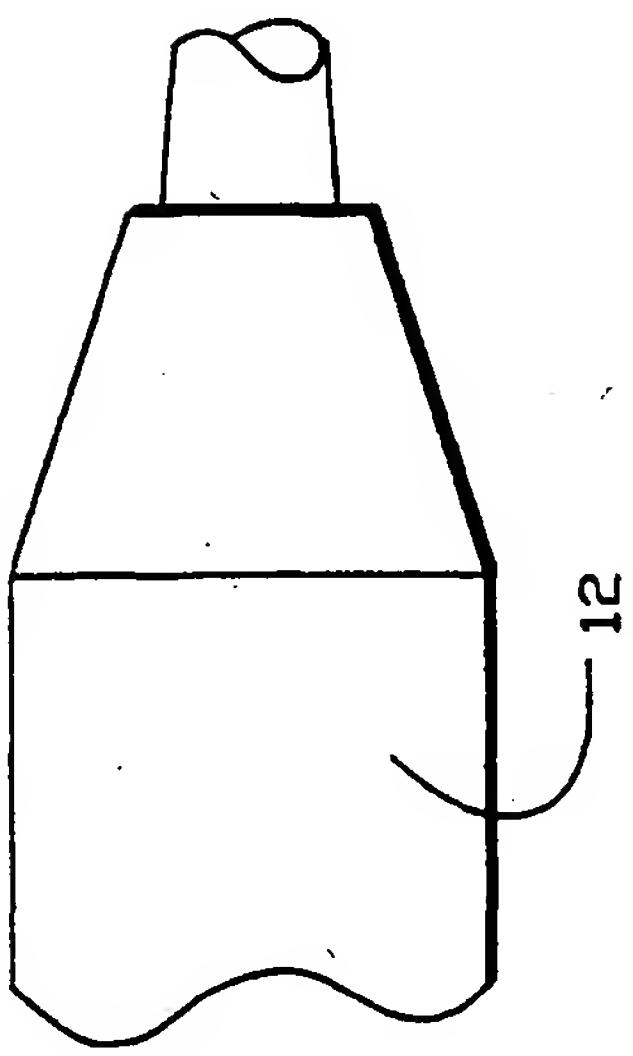


FIG. 6



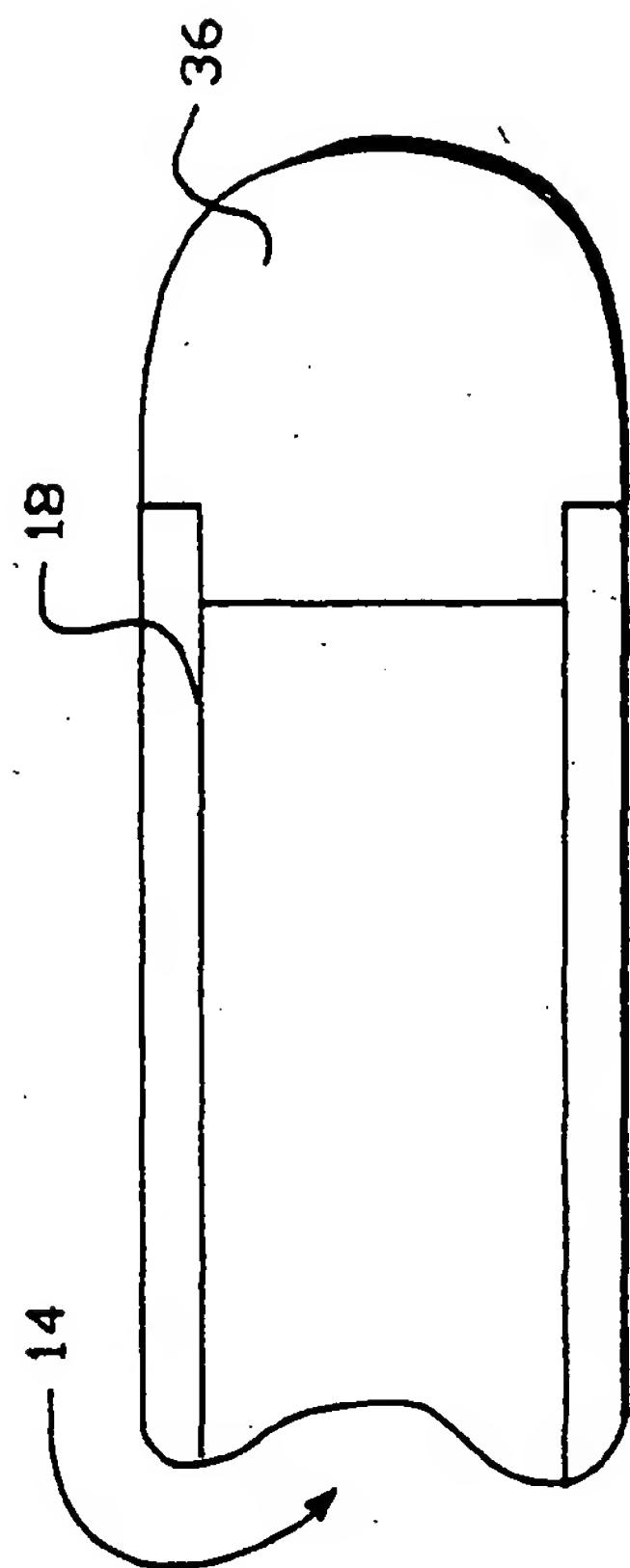


FIG. 8

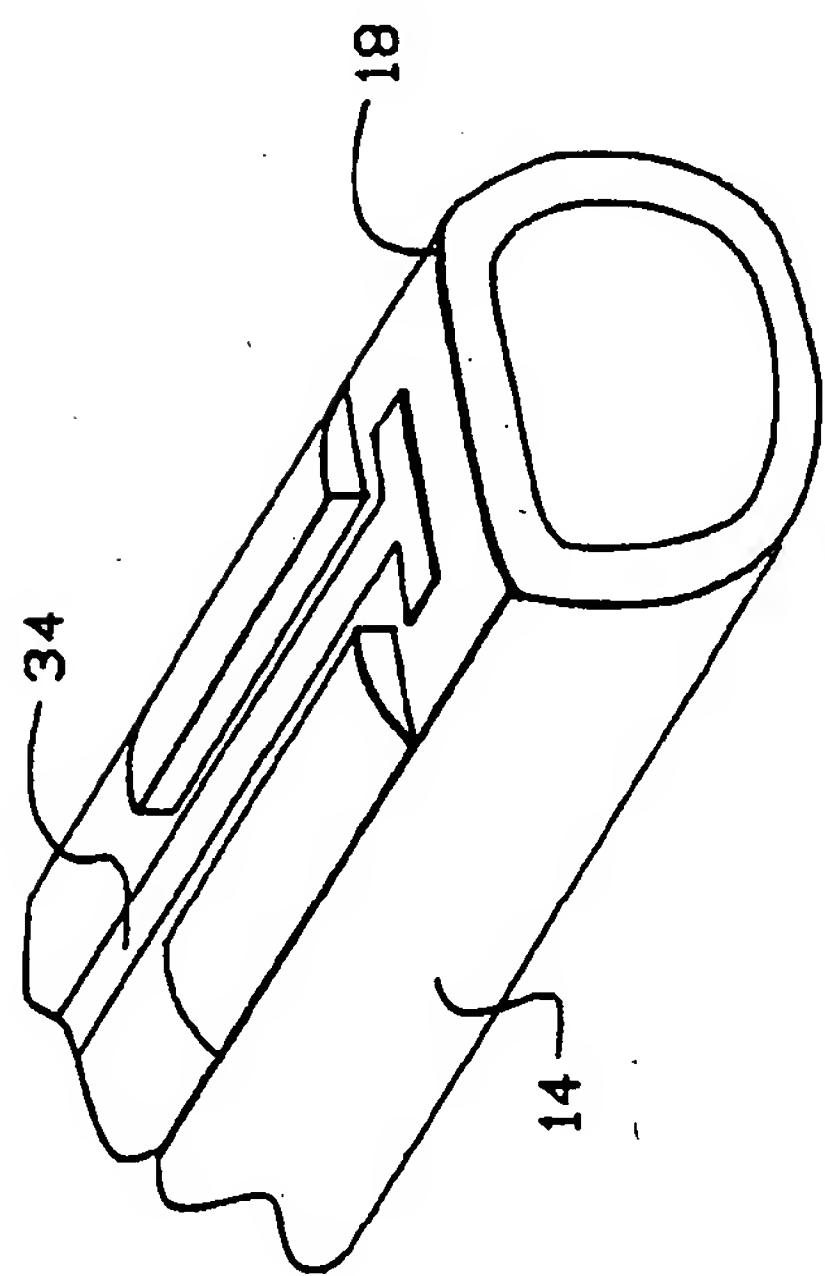


FIG. 7

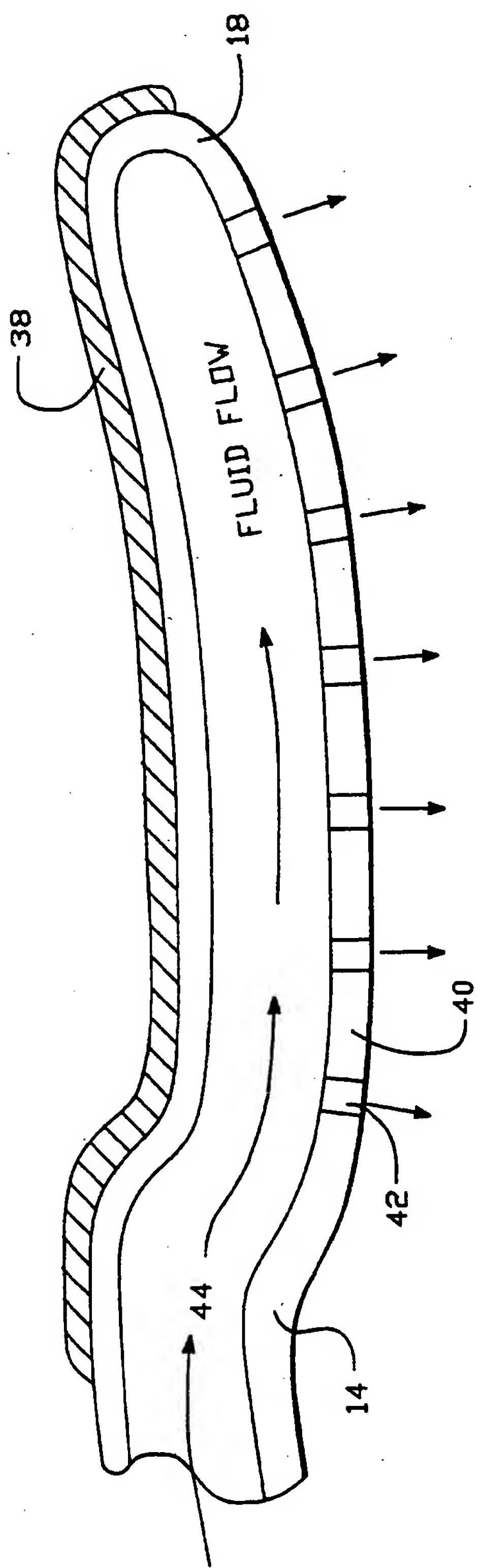


FIG. 9

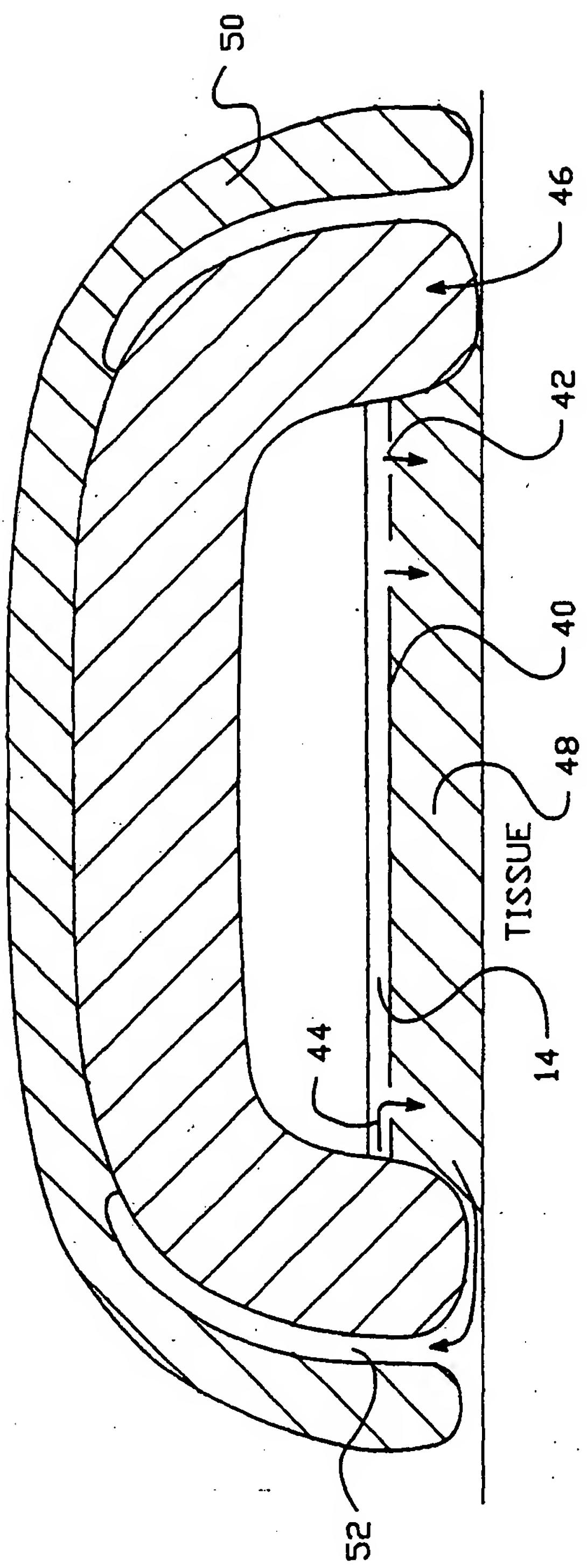


FIG. 10

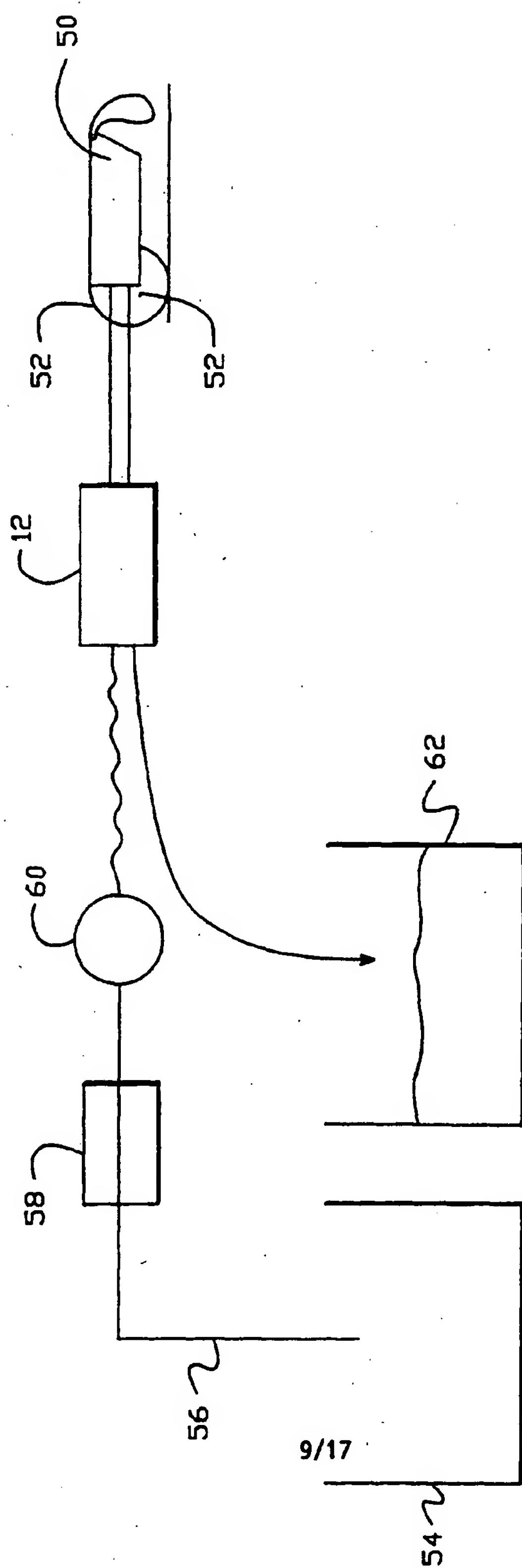


FIG. 11

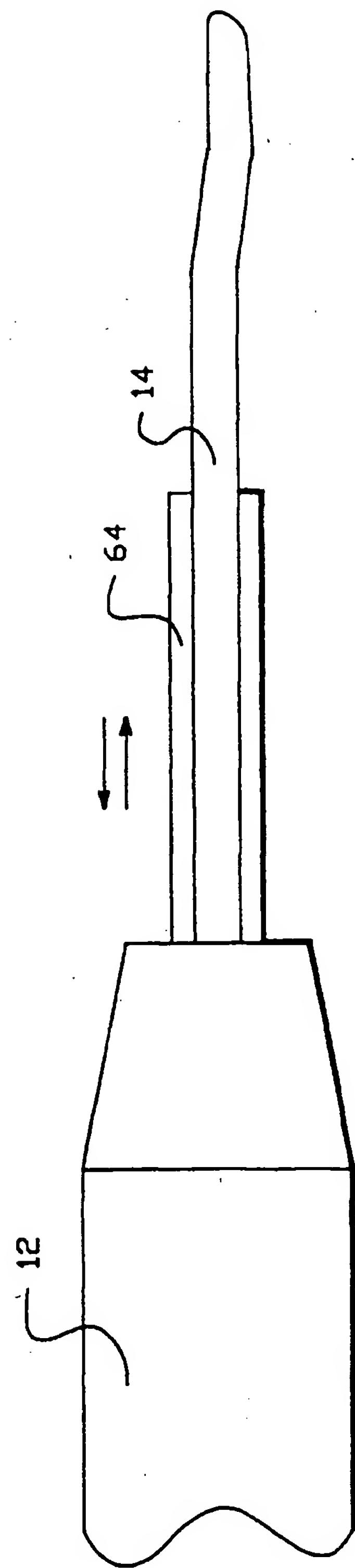


FIG. 12

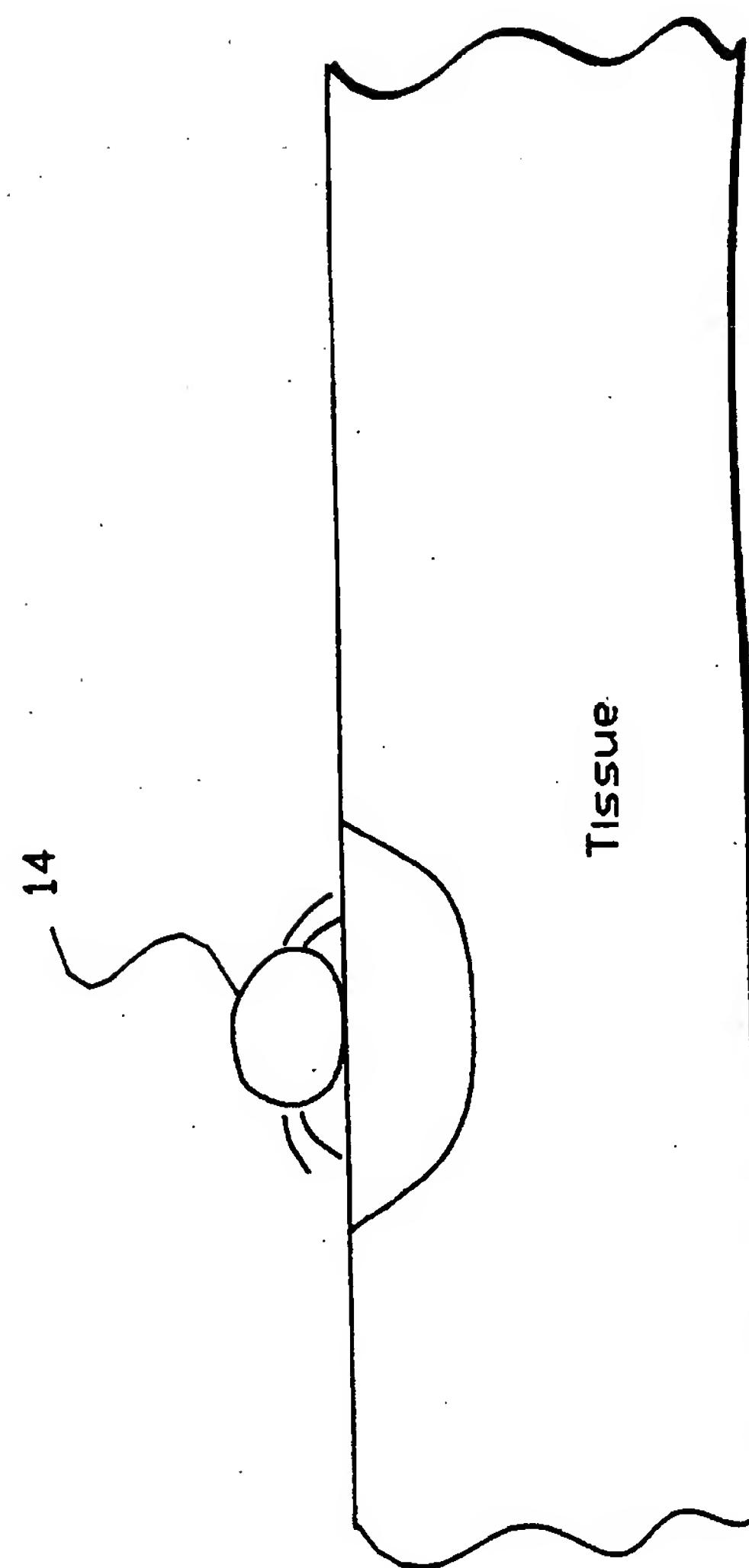


FIG. 13

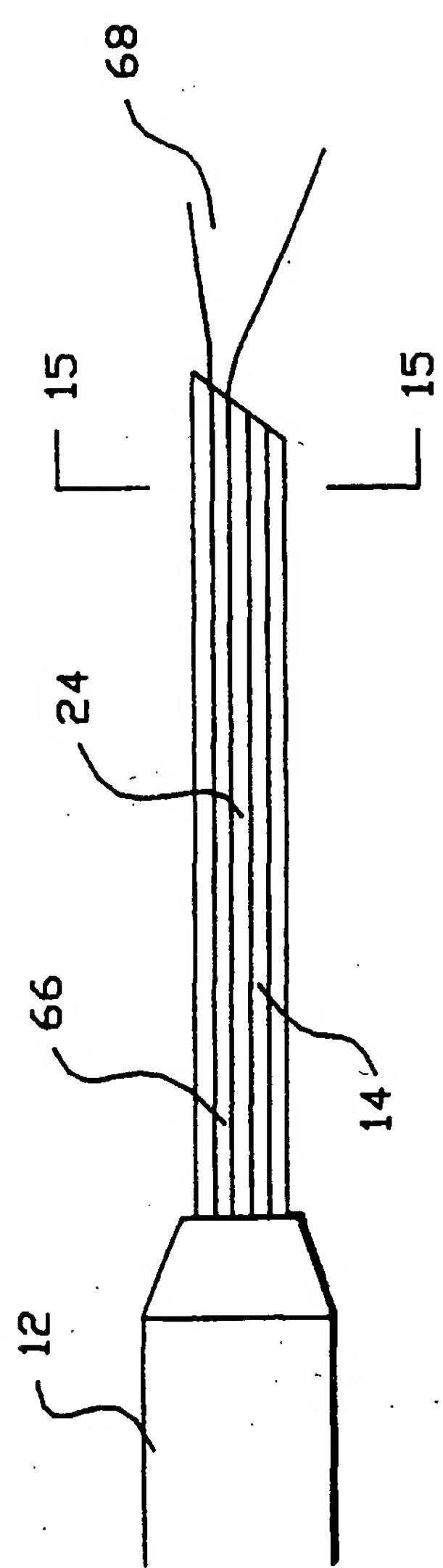


FIG. 14

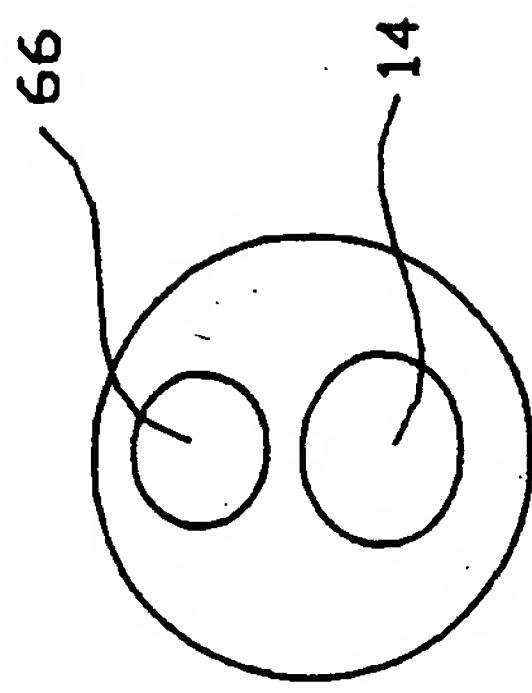


FIG. 15

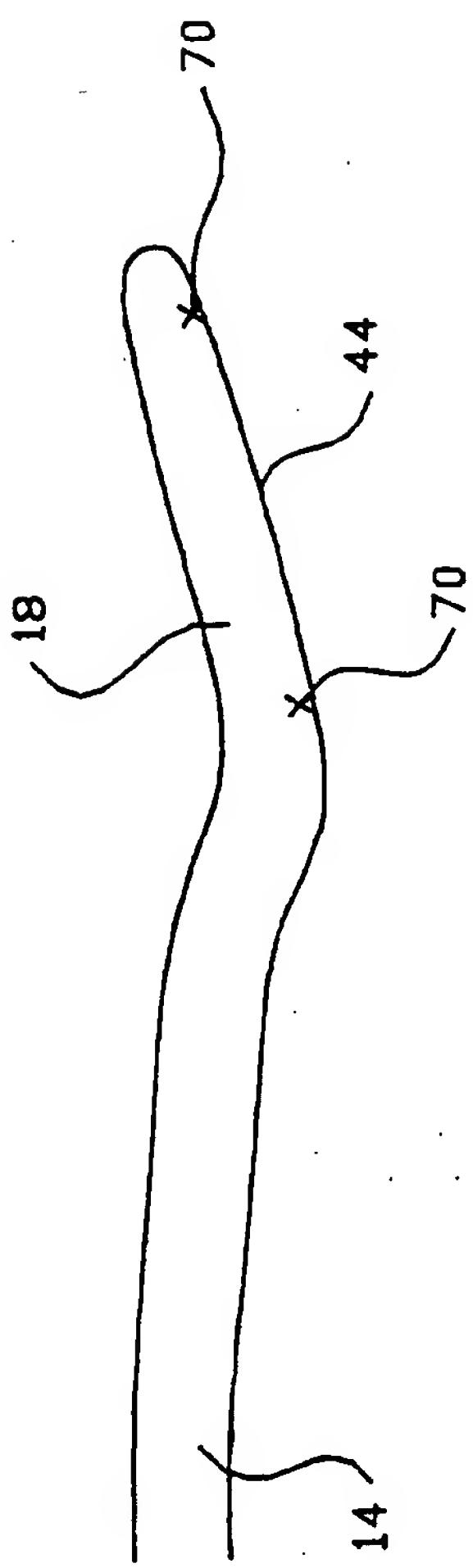


FIG. 16

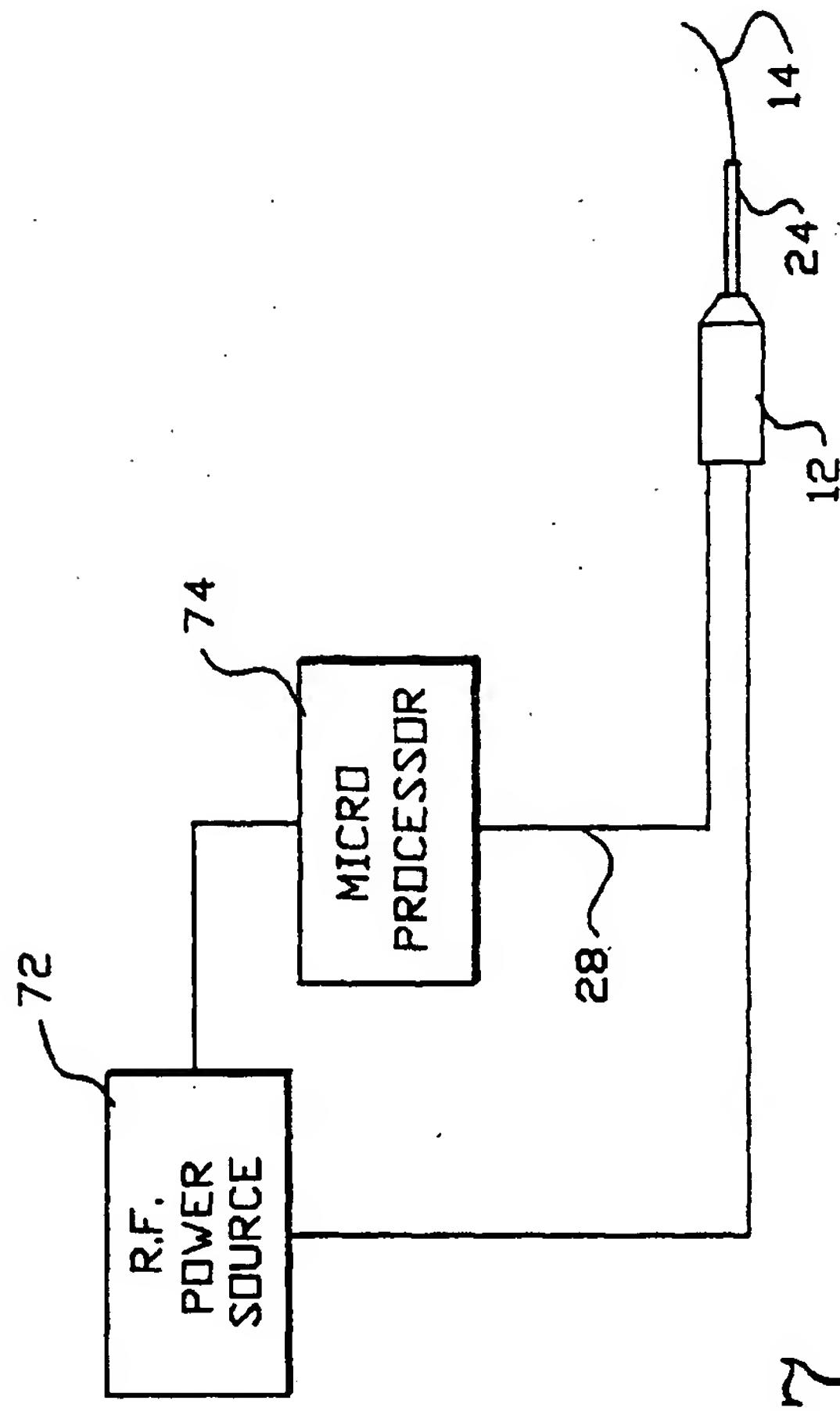


FIG. 17

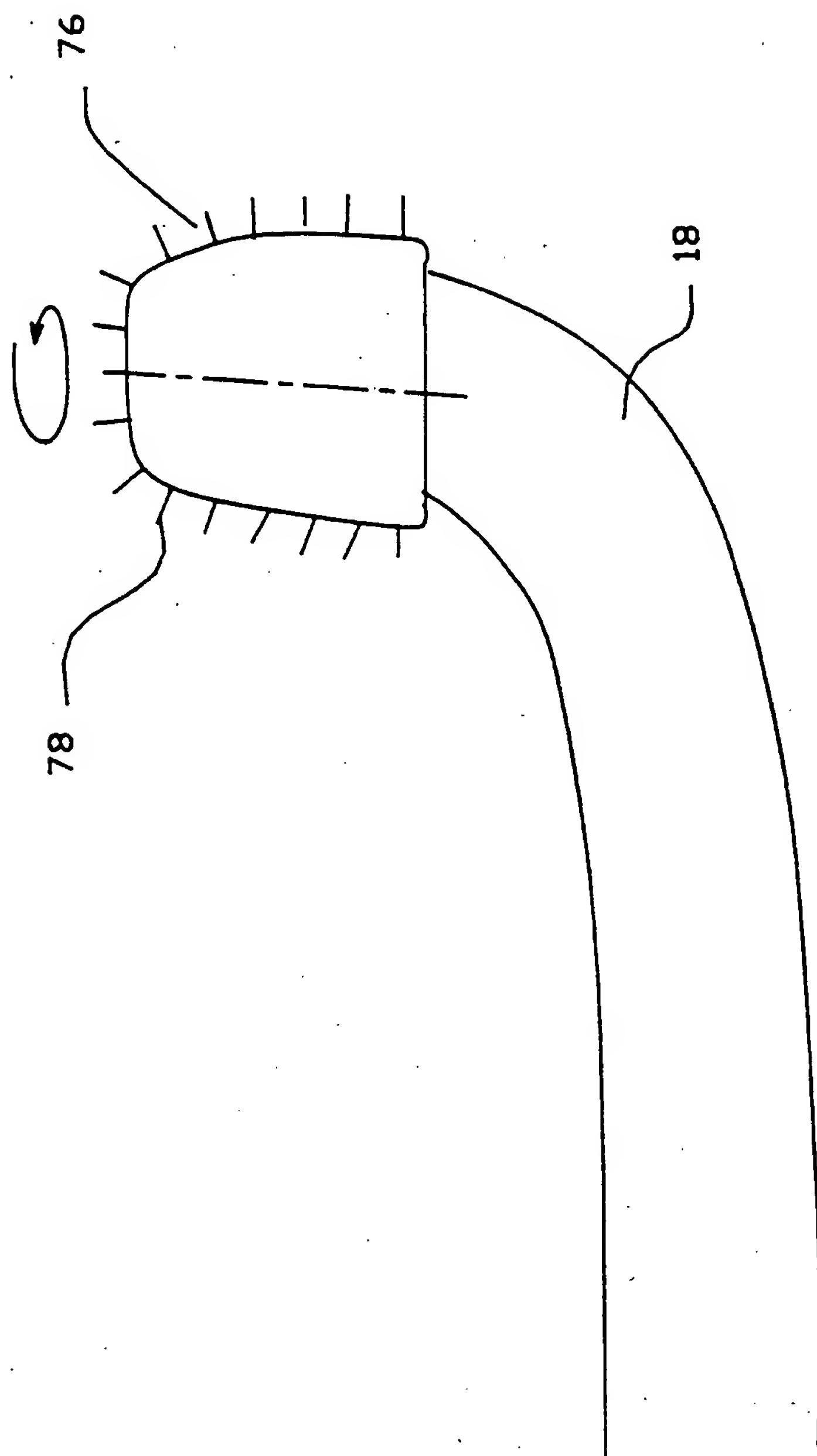
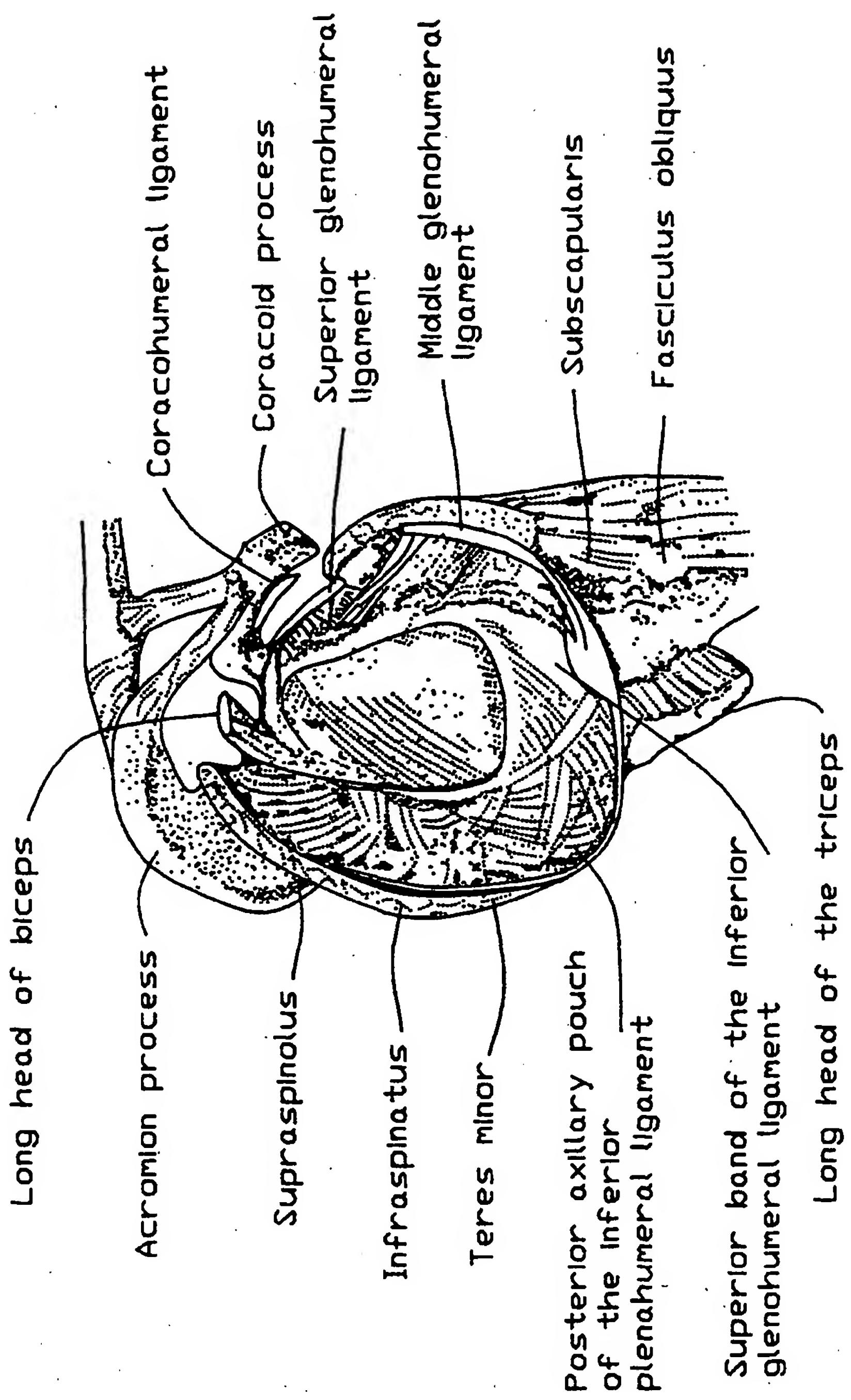


FIG. 18

FIG. 19



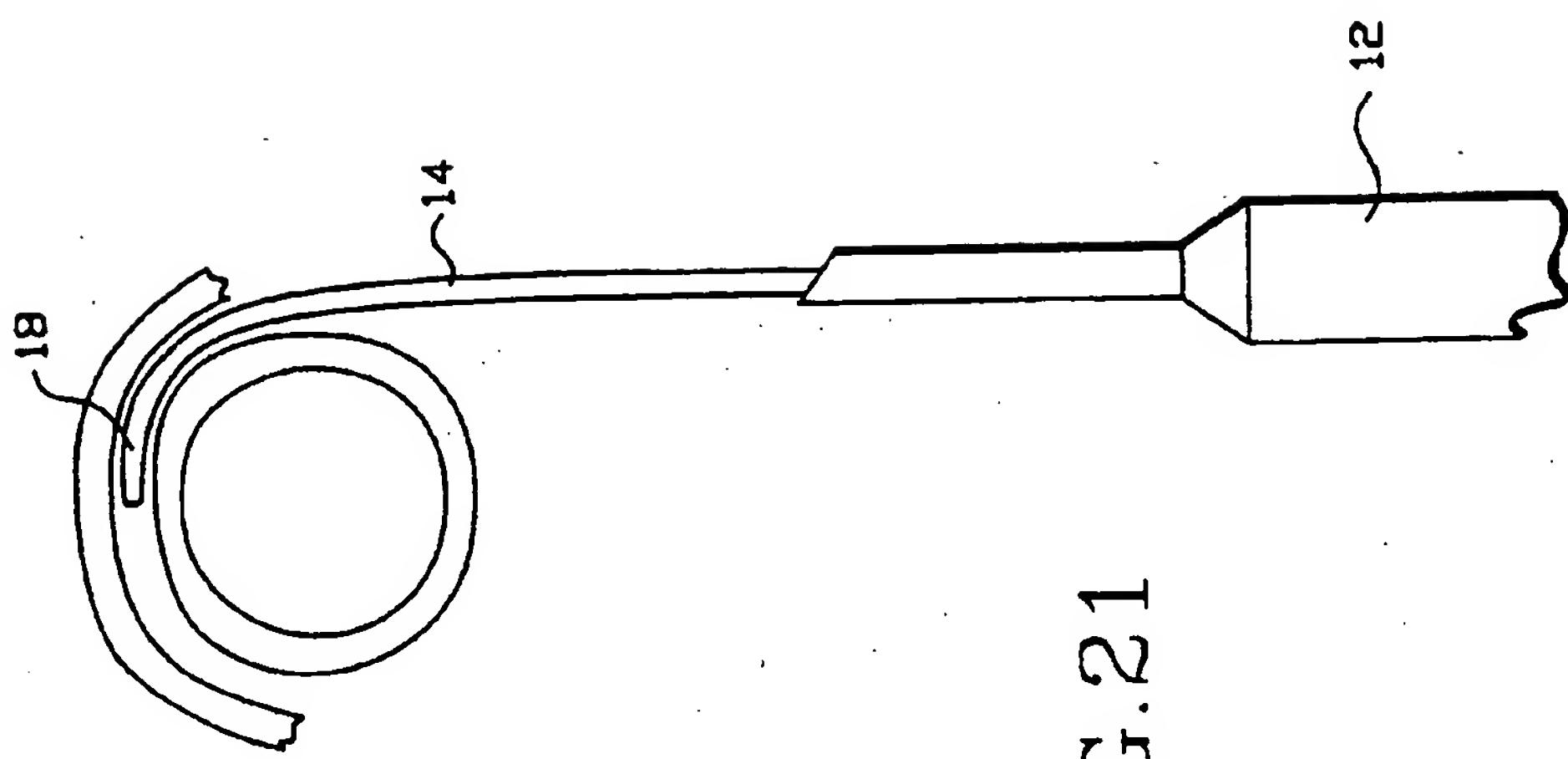


FIG. 21

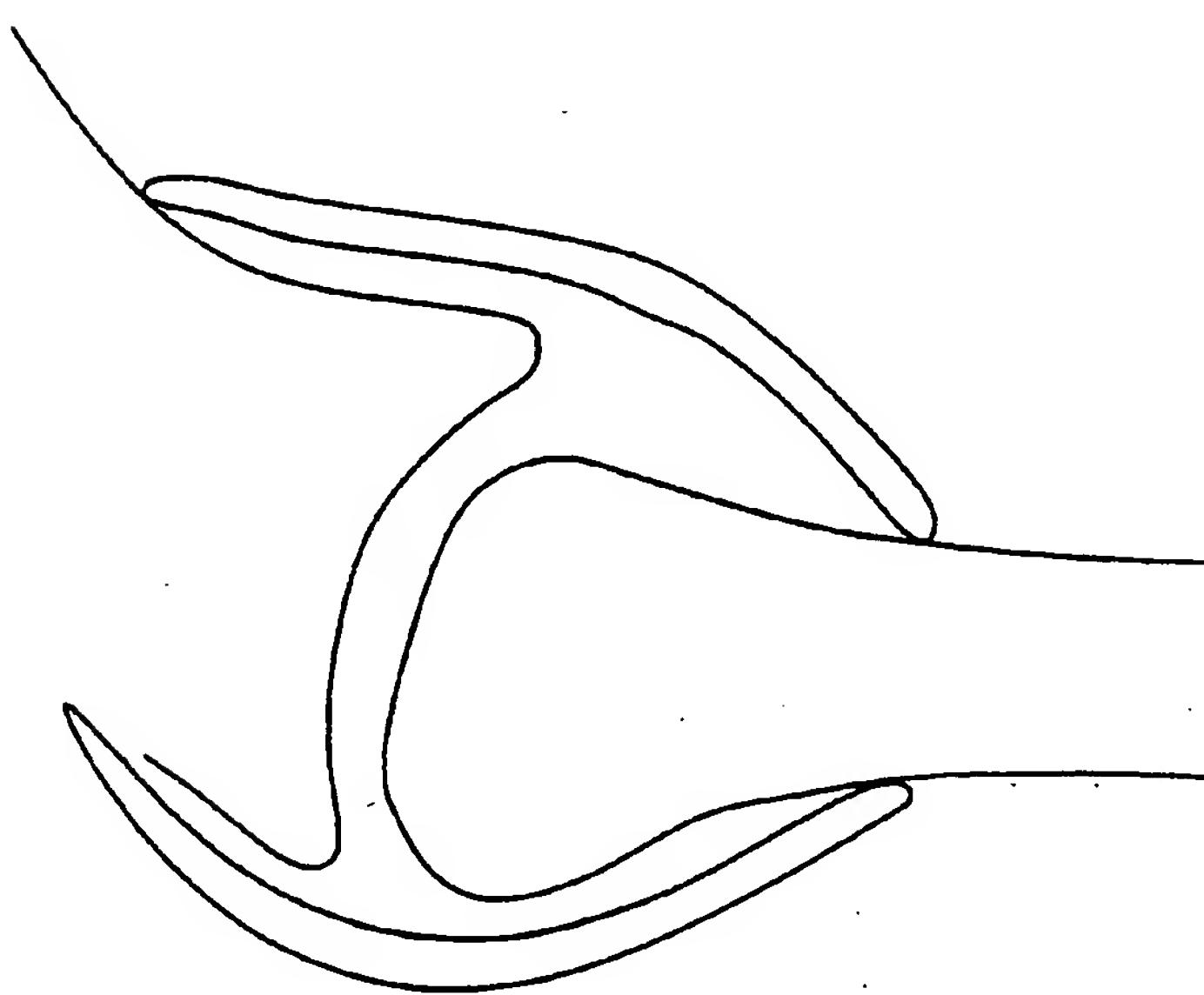


FIG. 20

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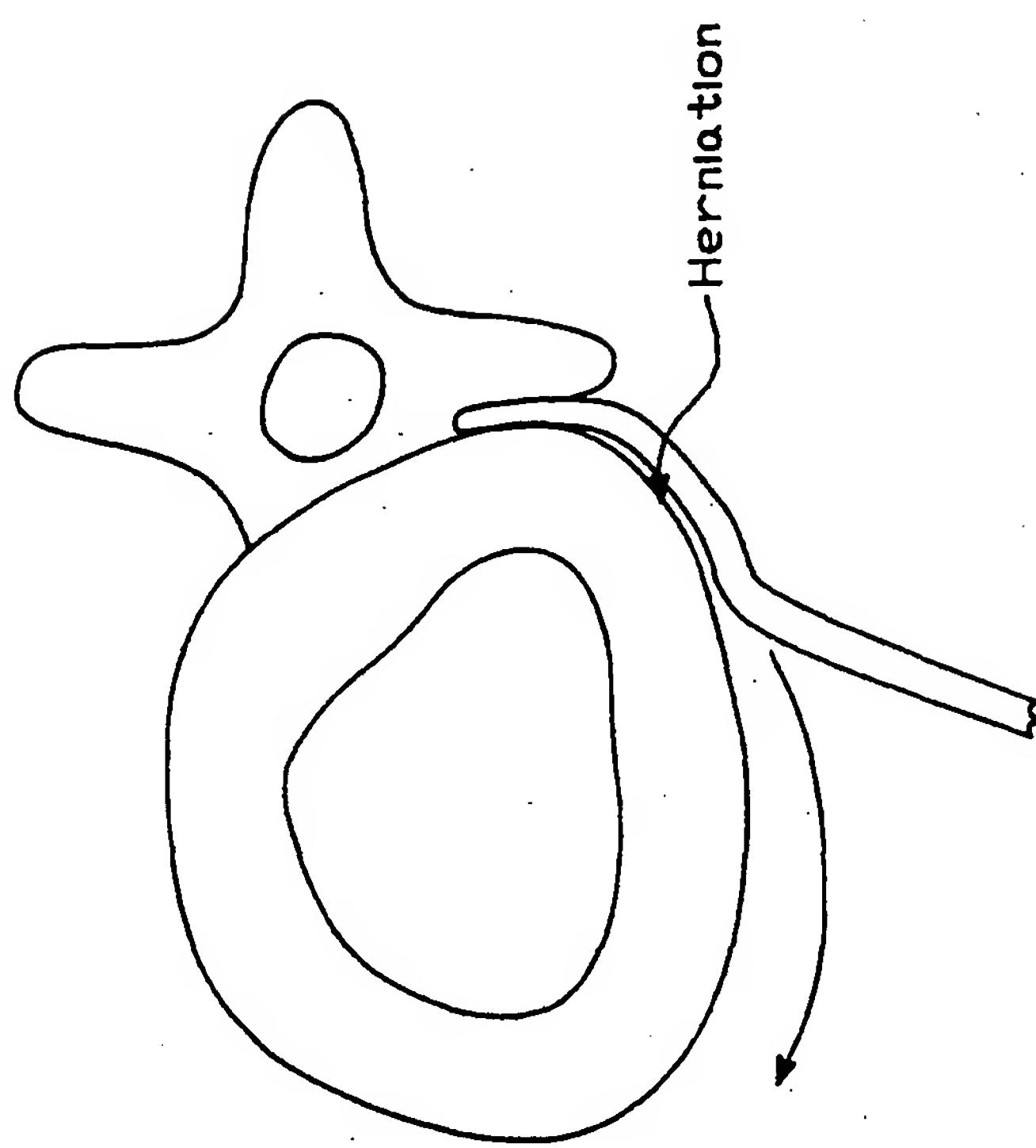


FIG. 23

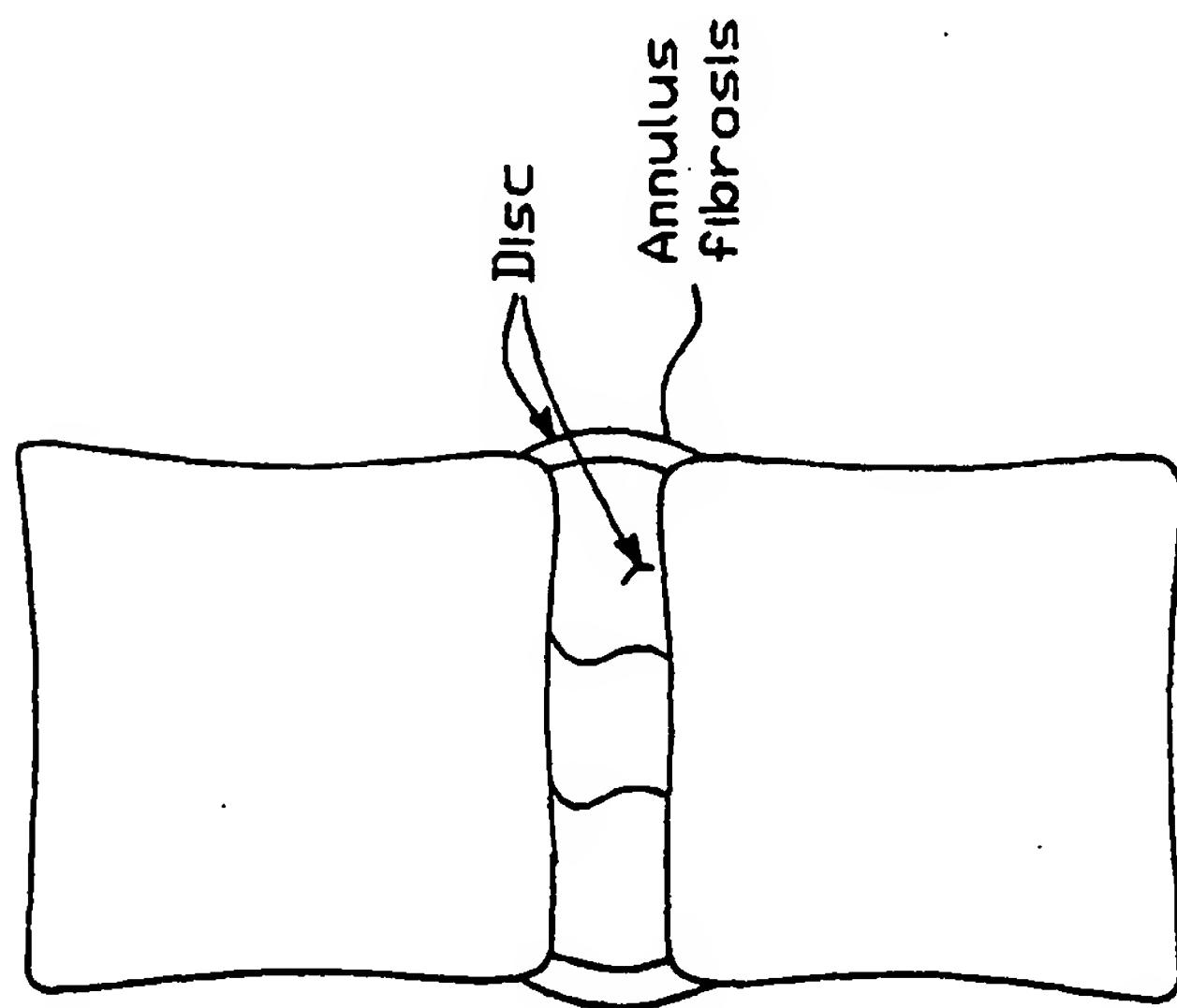


FIG. 22